

# Scroll wave drift Due to Anisotropy Gradients in the Cardiac Wall

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Snowbird DS19, 20 May 2019

# Outline

## ① Motivation

## ② Methods

- Response function framework
- Curved-space viewpoint
- Mean-field approach

## ③ Results

- Drift in the surface approximation
- 3D structure of the scroll wave core
- Finite thickness drift corrections

## ④ Conclusions

# Heart rhythm disorders: collective dynamics of non-linear waves

HEALTHY - PERTURBED - FAILING

# 3D dynamics in simulations of ventricular tachycardia

Cardiac excitation modeled as a reaction-diffusion process:

$$\partial_t \mathbf{u} = \partial_i (D^{ij}(\vec{r}) \partial_j \mathbf{P} \mathbf{u}) + \mathbf{F}(\mathbf{u}) \quad (1)$$

with  $u_1 \equiv V$  transmembrane potential.

# Questions

**Can we predict the drift of a rotor in the 3D cardiac wall from wall thickness and intramural fiber orientation?**

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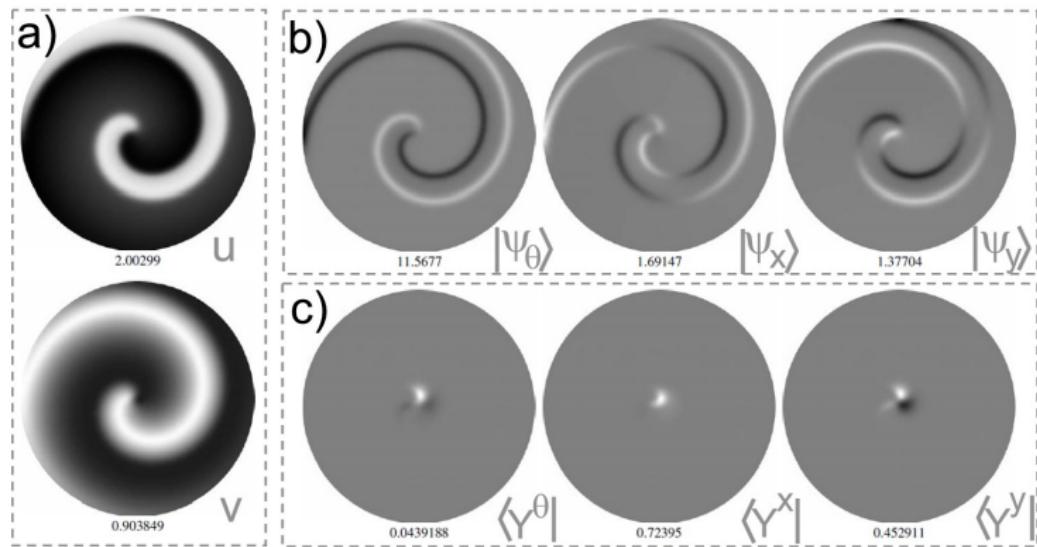
Finite thickness drift corrections

## ④ Conclusions

# Preliminaries: Particle-wave duality of spiral waves

$$\partial_t \mathbf{u} = \Delta \mathbf{P}\mathbf{u} + \mathbf{F}(\mathbf{u}) + \mathbf{h}(\vec{r}, t)$$

$$\partial_t X^m = v_0^m(\Phi) + \langle \mathbf{Y}^m | \mathbf{h} \rangle, \quad m \in \{X, Y, \Phi\}, \quad \langle \mathbf{f} | \mathbf{g} \rangle = \iint_{\mathbb{R}^2} \mathbf{f}^H \mathbf{g} d^2x$$



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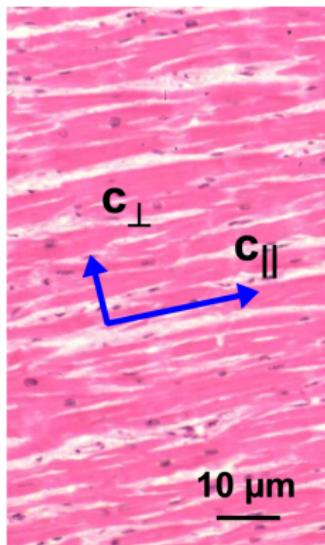
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# Preliminaries: Anisotropic wave propagation

If  $\det(\mathbf{D})$  constant and  $D^{ij} \equiv g^{ij}$ :

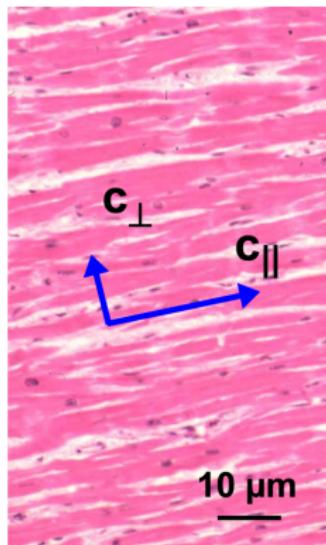
$$\partial_i (D^{ij}(\vec{r}) \partial_j V) = \frac{1}{\sqrt{g}} \partial_i (\sqrt{g} g^{ij} \partial_j V) = \mathcal{D}^2 V$$



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The heart is a Riemannian manifold

*Measuring distance in the heart using arrival time  
of traveling waves*

↔

Metric tensor  $\mathbf{g} = \mathbf{D}^{-1}$

$$ds^2 = g_{xx} dx^2 + 2g_{xy} dxdy + g_{yy} dy^2$$

Wellner et al. PNAS 2002;  
Verschelde et al. PRL 2007;  
Young et al. PNAS 2010

# How to rescale the spiral wave in every cross-section of a scroll wave ?

- ① Rescale axes according to in-plane conduction velocities?

$$x'_1 = x_1/c_1, \quad x'_2 = x_2/c_2 \quad (2)$$

*Setayeshgar & Bernoff, PRL 2002; Verschelde et al. PRL 2007*

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*Chapelle et al. Math. Models & Meth. Appl. Sci. 2013*

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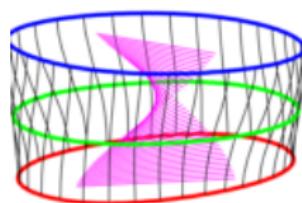
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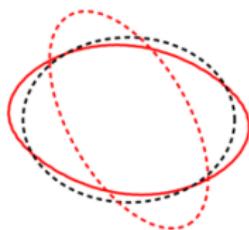
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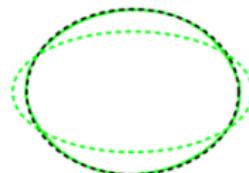
⇒ Numerical simulations in the Aliev-Panfilov model:



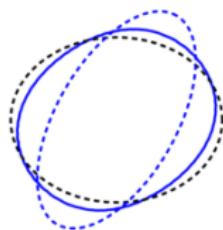
3D



epi



mid-wall



endo

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# A mean-field approximation to the diffusion tensor

- Define the thickness-average and its error:

$$\bar{f}(x, y) = \frac{1}{V} \int_0^L f(x, y, z) \sqrt{g} dz, \quad V = \int_0^L \sqrt{g} dz \quad (3)$$

$$\tilde{f}(x, y, z) = f - \bar{f} \quad (4)$$

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- We will need the **thickness-averaged diffusion tensor**

$$H^{ab}(x, y) = \overline{D^{ab}}, \quad a, b \in \{x, y\} \quad (5)$$

$$H_{ab} H^{bc} = \delta_a^c, \quad H = \det(H_{ab}) \quad (6)$$

$$D^{ab} = H^{ab} + \tilde{D}^{ab} \quad (7)$$

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- Thickness-averaged state variables:

$$\mathbf{u} = \bar{\mathbf{u}} + \tilde{\mathbf{u}} \quad (8)$$

# Limit of vanishing thickness

- Say the spatial decay constant of the RFs is  $d$
- If  $\epsilon = (L/d)^2 \ll 1$ , define relative depth  $\sigma = z/L \in [0, 1]$  and let  $\mathbf{u}(t, \tau)$  depend on time  $t$  and 'fast time'  $\tau = t/\epsilon$ :

$$\partial_t \mathbf{u} + \frac{1}{\epsilon} \partial_\tau \mathbf{u} = \partial_a (D^{ab} \partial_b \mathbf{P} \mathbf{u}) + \frac{1}{\epsilon} \mathbf{P} D^{zz} \partial_\sigma^2 \mathbf{u} + \mathbf{F}(\mathbf{u}). \quad (9)$$

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$$\partial_\tau \mathbf{u} = \mathbf{P} D^{zz} \partial_\sigma^2 \mathbf{u} \quad (10)$$

... there is only transmural diffusion!

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- In the limit of vanishing thickness,  $V$  is constant across the wall  
 $\Rightarrow \mathbf{u}$  is constant across the wall

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# Averaging of the RDE (1/2)

- ① Insert  $\mathbf{u} = \bar{\mathbf{u}} + \tilde{\mathbf{u}}$  and into the RDE assuming  $D^{xz} = D^{yz} = 0$ :

$$\begin{aligned}\partial_t \bar{\mathbf{u}} + \partial_t \tilde{\mathbf{u}} &= \frac{1}{\sqrt{g}} \partial_a (\sqrt{g} D^{ab} \partial_b \bar{\mathbf{u}}) + \frac{1}{\sqrt{g}} \partial_z (\sqrt{g} D^{zz} \mathbf{P} \partial_z \tilde{\mathbf{u}}) \\ &\quad + \frac{1}{\sqrt{g}} \partial_a (\sqrt{g} D^{ab} \partial_b \tilde{\mathbf{u}}) + \mathbf{F}(\bar{\mathbf{u}}) + \mathbf{F}'(\bar{\mathbf{u}}) \tilde{\mathbf{u}} + \mathcal{O}(\epsilon^2)\end{aligned}\quad (11)$$

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- ② Average over thickness:

$$\begin{aligned}\partial_t \bar{\mathbf{u}} &= \frac{1}{V} \partial_a (V H^{ab} \partial_b \bar{\mathbf{u}}) + \mathbf{F}(\bar{\mathbf{u}}) + \mathcal{O}(\epsilon). \\ &= \frac{1}{\sqrt{H}} \partial_a (\sqrt{H} H^{ab} \partial_b \bar{\mathbf{u}}) + \partial_a \ln(V/\sqrt{H}) H^{ab} \partial_b \bar{\mathbf{u}} + \mathbf{F}(\bar{\mathbf{u}}) + \mathcal{O}(\epsilon)\end{aligned}\quad (12)$$

⇒ Leading order: spiral ‘sees’ a curved surface with metric  $H^{ab}$ , with additional gradient term of the ‘potential’  $\ln(V/\sqrt{H})$ .

## Averaging of the RDE (2/2)

- ① Infinitesimal volume in a wall portion is  $Vdxdy = \sqrt{H}\mathcal{L}dxdy$ , so call  $\mathcal{L} = V/\sqrt{H}$  the 'effective filament length'.  
In simplest case:  $\mathcal{L} = L/\sqrt{D^{zz}}$ .

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- ② Introduce local Euclidean coordinates around the tip such that  $H^{ab} = \delta^{ab}$  and prescribe that  $\bar{\mathbf{u}} = \mathbf{u}_0$  in these coordinates

$$v^M = -\langle \mathbf{W}^M \mid \partial_a \ln \mathcal{L} H^{ab} \partial_b \mathbf{u}_0 \rangle, \quad M \in \{x, y, \phi\}, \quad a, b \in \{x, y\}$$

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- ③ After averaging over one rotation:

$$v^a = -\gamma_1 D^{ab} \partial_b \ln \mathcal{L} - \gamma_2 \frac{\epsilon^{ab}}{\sqrt{H}} \partial_b \ln \mathcal{L} \quad (13)$$

where  $\gamma_1 = \frac{1}{2} \langle \mathbf{W}^a | \mathbf{P} \partial_a \mathbf{u}_0 \rangle$ : filament tension

# Result for a filament in a wedge with opening angle $\beta$

- If  $D^{ij} = \delta^{ij}$ , then

$$\begin{aligned}V &= \int \sqrt{g} ds = \beta r = L \\H^{ab} &= \frac{1}{V} \int \sqrt{g} \delta^{ab} ds = \delta^{ab} \\\sqrt{H} &= 1 \\\mathcal{L} &= L = \beta r\end{aligned}\tag{14}$$

so 'effective filament length'  $\mathcal{L}$  here equals the usual filament length  $L$

- Equation of motion becomes:

$$\begin{aligned}v^a &= -\frac{\gamma_1}{r} \vec{e}_r + \frac{\gamma_2}{r} \vec{e}_y \\\Rightarrow \vec{v} &= \gamma_1 k \vec{N} + \gamma_2 k \vec{B}.\end{aligned}\tag{15}$$

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- We recover the result from Biktashev, Holden & Zhang (1994)

# Result for rotational anisotropy

- With myofiber direction  $\vec{e}_f = \cos \alpha \vec{e}_x + \sin \alpha \vec{e}_y$ ,  
and total fiber rotation angle  $\Theta$  over myocardial wall of thickness  $L$ :

$$\alpha(z) = \alpha_0 + \Theta \cdot (z - L/2) \quad (16)$$

- From  $D^{ij} = D_2 \delta^{ij} + (D_1 - D_2) e_f^i e_f^j$ , with  $\alpha_0 = 0$ , it follows that

$$(H^{ab}) = (\overline{D}^{ab}) = \begin{pmatrix} D_m + D_a \frac{\sin \Theta}{\Theta} & 0 \\ 0 & D_m - D_a \frac{\sin \Theta}{\Theta} \end{pmatrix} \quad (17)$$

$$1/H = \det(H^{ab}) = D_m^2 - D_a^2 \frac{\sin^2 \Theta}{\Theta^2} \quad (18)$$

where  $D_m = (D_1 + D_2)/2$ ,  $D_a = (D_1 - D_2)/2$ .

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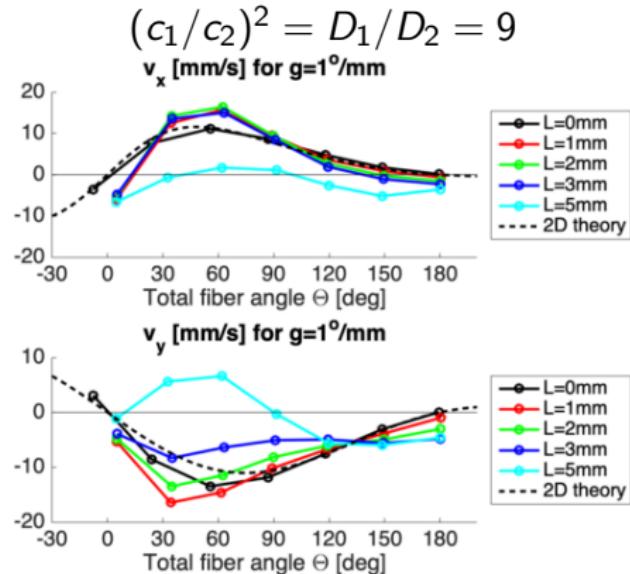
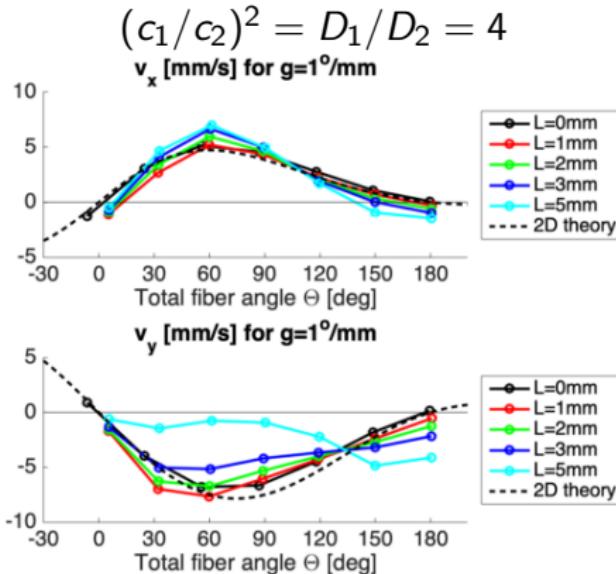
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where  $D_m = (D_1 + D_2)/2$ ,  $D_a = (D_1 - D_2)/2$ .

- For  $\gamma_1 > 0$ , the scroll wants to minimize effective filament length:  
 $\mathcal{L} \downarrow \Leftrightarrow 1/H \downarrow \Leftrightarrow \text{sinc}^2 \Theta \uparrow \Leftrightarrow |\Theta| \downarrow$  in  $(0, \pi)$ 
  - For  $\gamma_1 > 0$ , spirals drift to region with smallest fiber rotation
  - For  $\gamma_1 < 0$ , spirals drift to region with largest fiber rotation

# Comparison of 2D theory with 2D and 3D simulations



- Aliev-Panfilov model  $a = 0.15, k = 8, \epsilon = 0.002, \mu_1 = 0.2, \mu_2 = 0.3$
- Total fiber rotation angle  $\Theta = \Theta(0) + gx$
- Good correspondence with theory for  $L \leq 3$  mm,  $g \leq 1^\circ / \text{mm}$

# What did we neglect?

- Recall that  $D^{ab} = H^{ab} + \tilde{D}^{ab}$ ;  $\mathbf{u} = \bar{\mathbf{u}} + \tilde{\mathbf{u}}$ , so for constant  $V$ :

$$\begin{aligned}\overline{\partial_a(D^{ab}\partial_b\mathbf{u})} &= \overline{\partial_a(H^{ab}\partial_b\bar{\mathbf{u}})} + \overline{\partial_a(\tilde{D}^{ab}\partial_b\bar{\mathbf{u}})} + \overline{\partial_a(H^{ab}\partial_b\tilde{\mathbf{u}})} \\ &\quad + \overline{\partial_a(\tilde{D}^{ab}\partial_b\tilde{\mathbf{u}})}\end{aligned}\tag{19}$$

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- Part of  $\tilde{\mathbf{u}}$  can be captured by dynamics of the scroll wave filament  $[X(z, t), Y(z, t), \Phi(z, t)]$ :

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- What is the shape of the scroll wave core in a thin anisotropic slab?

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# Analytical solution for the scroll wave core (1/2)

For rotational anisotropy with fiber direction  $\alpha(z)$  independent of  $x, y$ :

- ① Rescale  $x, y$  such that  $H^{ab} = \delta^{ab}$  such that

$$X^a = X_0^a(\Phi) + R_A^a(\Phi)x^A, \quad X^\phi = \Phi(t) + \phi(t), \quad \Phi(t) = \omega t \quad (21)$$

- ② Take  $\mathbf{u}(x, y, z, t) \approx \mathbf{u}_0(X^\mu(z, t), x, y) + \mathbf{u}_1 + \mathcal{O}(\epsilon^2)$
- ③ Keep leading order and project onto RFs to find:

$$\partial_t x^M - iM\omega x^M - P_N^M \partial_z^2 x^N = Q_{AB}^M \tilde{D}^{AB}(\Phi, z) + \mathcal{O}(\epsilon^2) \quad (22)$$

where

$$P_N^M = \langle \mathbf{W}^M | \mathbf{P} \partial_N \mathbf{u}_0 \rangle, \quad Q_{AB}^M = \langle \mathbf{W}^M | \mathbf{P} \partial_{AB}^2 \mathbf{u}_0 \rangle \quad (23)$$

- ④ Eq. (22) is a periodically driven linear PDE with known source

$$\tilde{D}^{ab}(\Phi, z) = \sum_{k=1}^{\infty} \sum_{\ell=-2,0,2} D_{k,\ell}^{ab} \cos(kz) e^{i\ell\Phi} \quad (24)$$

## Analytical solution for the scroll wave core (2/2)

- ⑤ Also write filament shape  $x^a$  in a double Fourier series:

$$x^a(\Phi, z) = \sum_{k=1}^{\infty} \sum_{\ell=-2,0,2} x_{k,\ell}^a \cos(kz) e^{i\ell\Phi} \quad (25)$$

- ⑥ Then, Fourier components for the shape of the scroll wave core are found from solving linear  $3 \times 3$  systems, for  $k \in \mathbb{N}$ ,  $\ell \in \{-2, 0, 2\}$ :

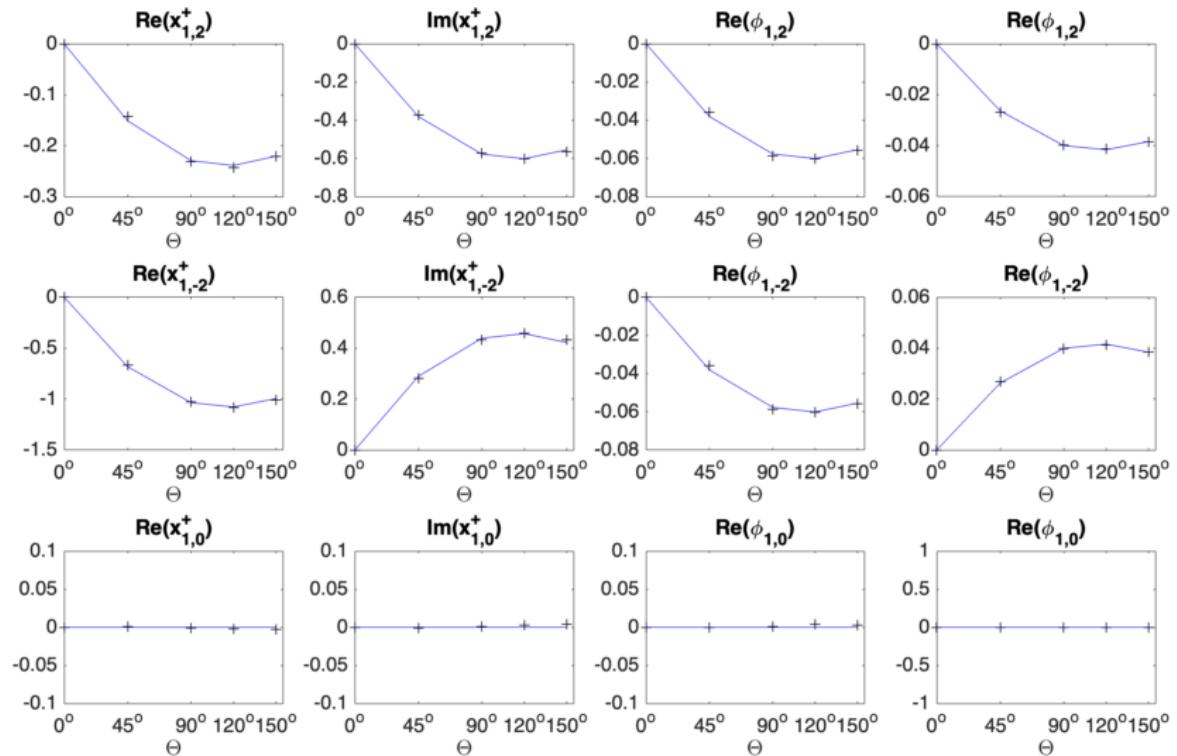
$$[i(\ell - M)\omega \delta_N^M + k^2 P_N^M] x_{k,\ell}^N = \sum_{\substack{a,b \in \{-1,1\} \\ a+b=\ell}} Q_{ab}^M D_{k,\ell}^{ab}. \quad (26)$$

using the complex basis: if  $Z^\pm = -(x \pm iy)$ , then

$$\begin{aligned} \mathbf{W}^{\pm 1} &= -(\mathbf{W}^x + i\mathbf{W}^y), & \mathbf{V}_{\pm 1} &= -\frac{1}{2}(\partial_x \mathbf{u}_0 - i\partial_y \mathbf{u}_0) \\ D^{++} &= (D^{xx} - D^{yy}) + 2iD^{xy}, & D^{+-} &= D^{xx} + D^{yy} \end{aligned}$$

# Fit of core shape vs. anisotropy in Fourier space

We expect that  $x_{k,a+b}^\mu \propto D_k^{ab}(\Theta)$  for given  $L$ :



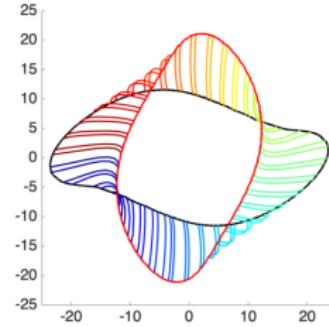
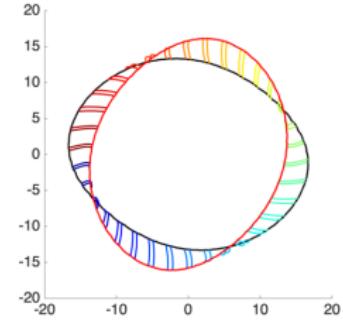
# Fit of core shape vs. anisotropy

$$L = 1\text{cm}$$

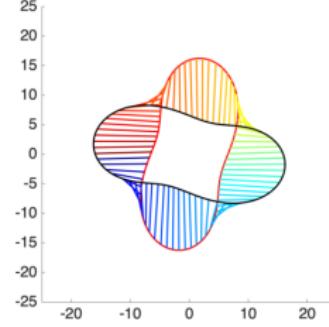
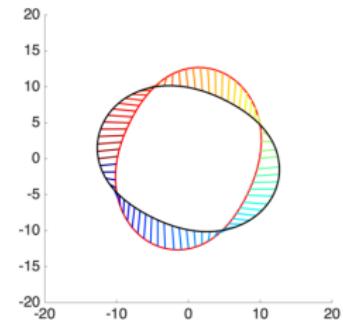
$$D_1/D_2 = 4$$

$$D_1/D_2 = 9$$

Simulation



Theory



(theory includes only modes with  $k = 0, 1$ ,  $\ell = -2, 0, 2$ )

# Outline

## ① Motivation

## ② Methods

- Response function framework
- Curved-space viewpoint
- Mean-field approach

## ③ Results

- Drift in the surface approximation
- 3D structure of the scroll wave core
- Finite thickness drift corrections

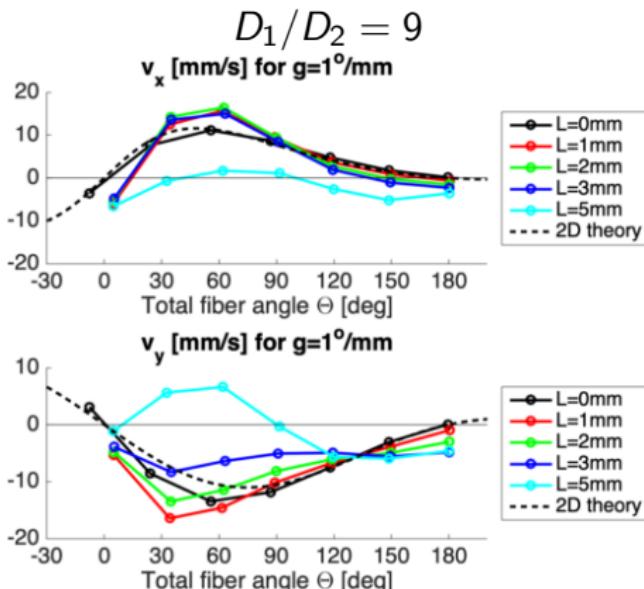
## ④ Conclusions

## And finally: finite thickness corrections to rotor drift

Average the perturbation term over  $\Phi$  and  $z$ :

$$\begin{aligned} V^c &= \frac{1}{2\pi} \oint d\Phi \langle \mathbf{W}^c | \mathbf{P} \overline{\partial_a(\tilde{D}^{ab} \partial_b \tilde{\mathbf{u}})} \rangle \\ &= \frac{1}{2\pi} \oint d\Phi \langle \mathbf{W}^c | \mathbf{P} \overline{\partial_a(\tilde{D}^{ab} x^m \partial_{bm}^2 \mathbf{u}_0)} \rangle \\ &= \frac{1}{2\pi} \oint d\Phi Q_{bm}^c(\Phi) \overline{F^b x^m}, \quad \text{with } \partial_a D^{ab} = F^b \\ &= \sum_{k=1}^{\infty} \frac{1}{2\pi} \oint d\Phi Q_{bm}^c(\Phi) F_k^b x_k^m(\Phi) \\ &= \sum_{k=1}^{\infty} \sum_{b+m-c=\ell} Q_{bm}^c F_k^b x_{k,\ell}^m \\ &= \sum_{k=1}^{\infty} \sum_{b+m-c=\ell} Q_{bm}^c A_{nk}^m Q_{ad}^n D_{kl}^{ad} F_k^b \quad \text{since } x_k^m = A_{kn}^m Q_{ad}^n D_{kl}^{ad} \end{aligned}$$

# Finite thickness corrections to rotor drift in rotational anisotropy



Next steps:

- Predict cases from knowledge of  $P_n^m$ ,  $Q_{nl}^m$
- Quadratic theory to handle  $L > 3$  mm
- Case of meander:  $P_n^m(\Psi)$  where  $\Psi$  is phase of meander
- Detailed ionic models

# Conclusions

If [decay length of spiral sensitivity] / [cardiac wall thickness]  $\ll 1$ :

- Scroll wave ‘sees’ a surface with  $H^{ab} = \overline{D}^{ab}$
- Leading order dynamics for circular-core spirals is

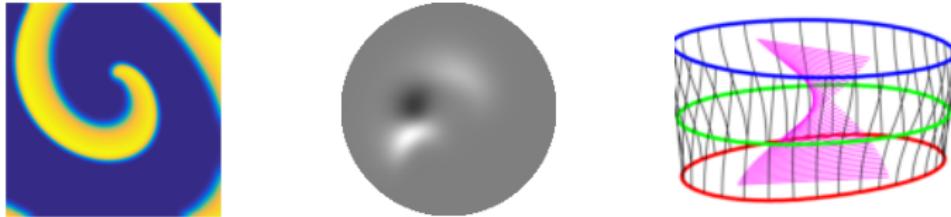
$$\dot{X}^a = - [\gamma_1 H^{ab} + \gamma_2 \frac{\epsilon^{ab}}{\sqrt{H}}] \partial_b \ln \mathcal{L} \quad \text{Dierckx SIAM 2019}$$

$$- [q_1 H^{ab} + q_2 \frac{\epsilon^{ab}}{\sqrt{H}}] \partial_b \mathcal{R} \quad \text{Dierckx et al. PRE 2013}$$

$\mathcal{R}$ : Ricci scalar using metric  $H^{ab}$

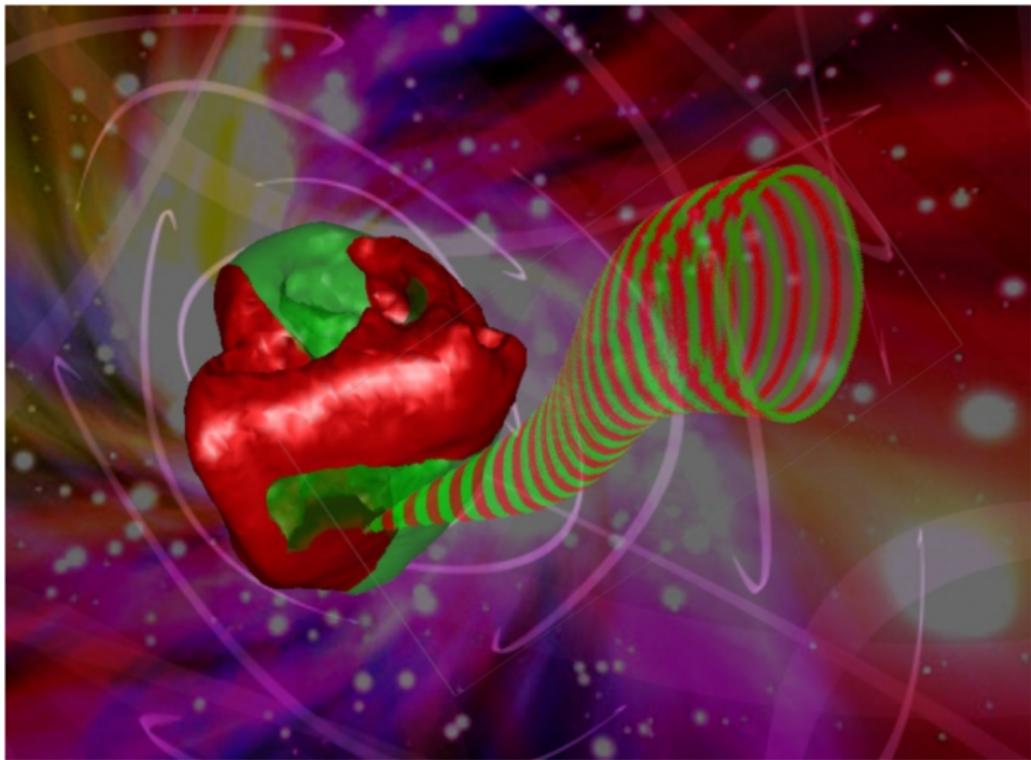
$L$ : medium thickness or effective filament length, using metric  $D^{ab}$

- Fourier series solution was found for the shape of the scroll wave core



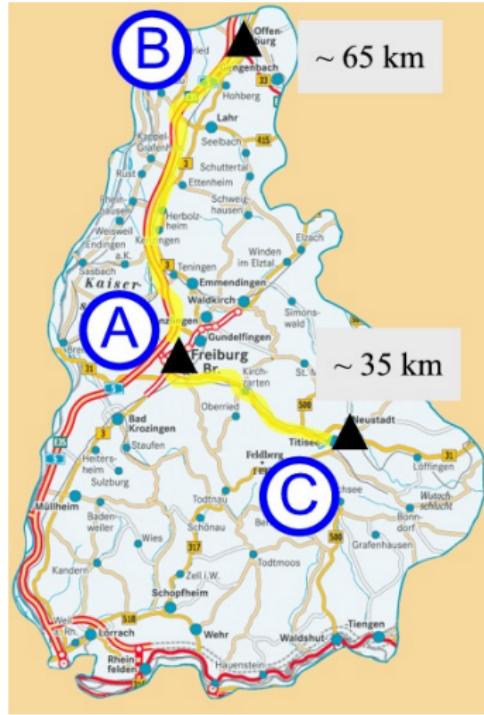
# More talks from people in cardiac modeling:

- Tue 4pm, Superior A: Roman Grigoriev  
Discovery of High-order PDE models with latent variables
- Wed 9:15, Maybird: Shreya Segal  
Bifurcation Analysis of spiral waves
- Wed 5pm-6:40, Maybird: MS 156  
Lightning-fast interactive simulations of reaction-diffusion systems  
Abouzar Kaboudian, Shahriar Iravanian, Yanyan Ji, Hector Velasco Perez
- Thu 8:55am, Ballroom 2: Laura Munoz  
Prediction of Abnormal Cardiac Rhythms with a 1D Dynamical Model
- Thu 3:35pm, Ballroom 3: Philipp Kuegler  
Multiple Time Scale Analysis of Early Afterdepolarizations in Cardiac Action Potentials



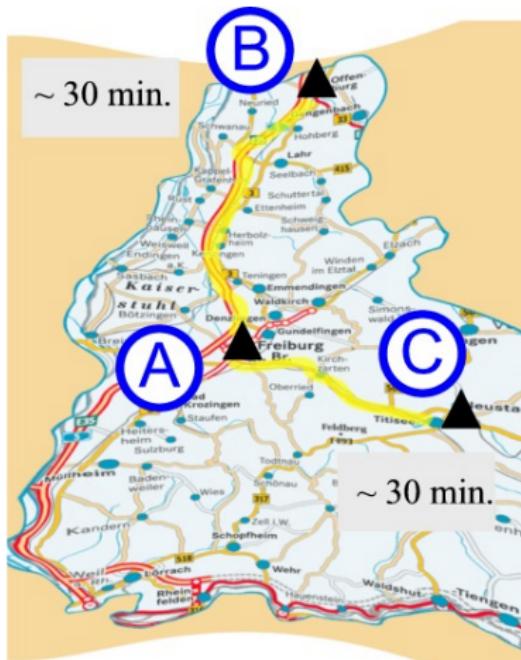
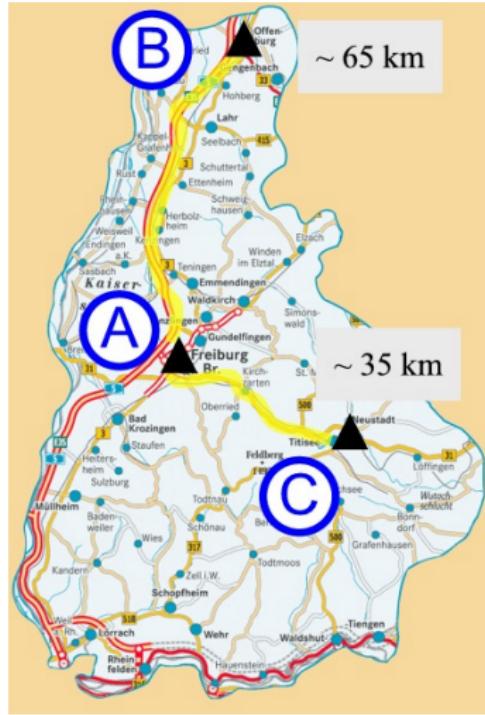
# The road map analogy

Is place C closer to A than B?



# The road map analogy

Is place C closer to A than B?



Both B and C have the same travel time from A!