

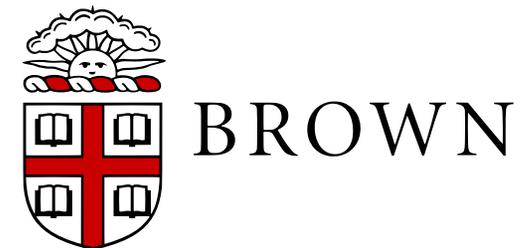
# SIMULATIONS OF VISCOUS SUSPENSION FLOWS WITH A MESHLESS MLS SCHEME

Amanda Howard<sup>1</sup>   Martin Maxey<sup>1</sup>   Nathaniel Trask<sup>2</sup>

<sup>1</sup>Division of Applied Mathematics, Brown University

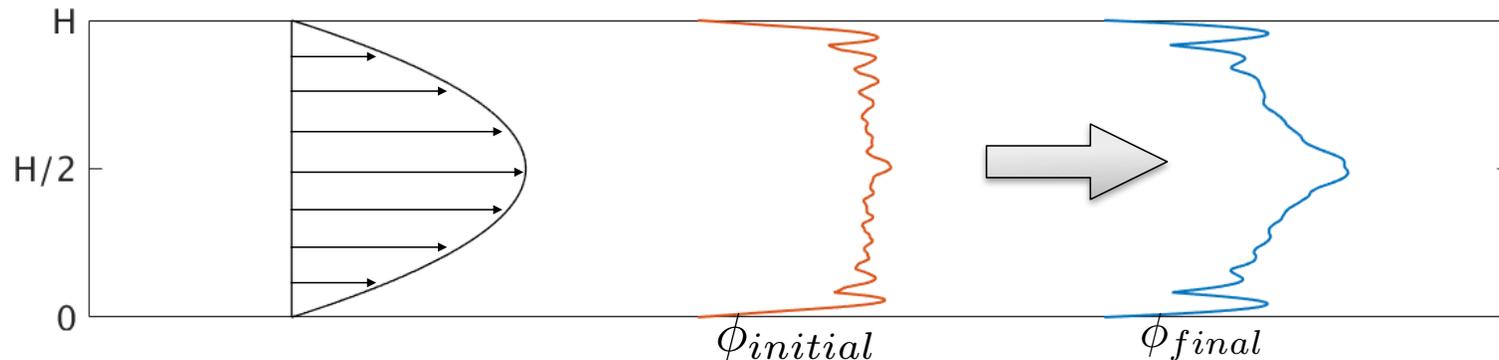
<sup>2</sup>Sandia National Laboratories

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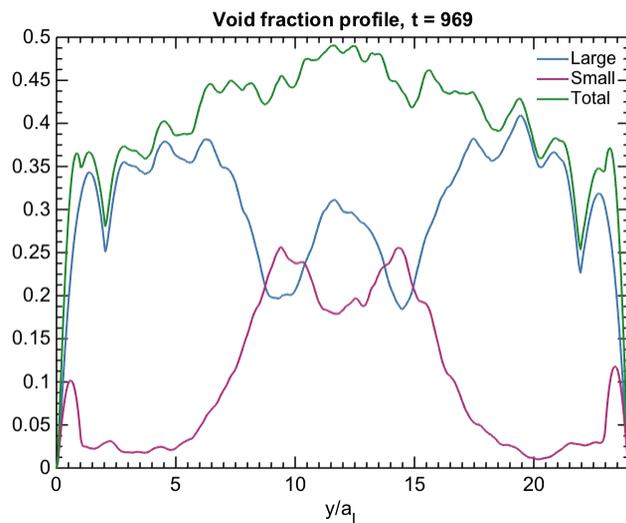
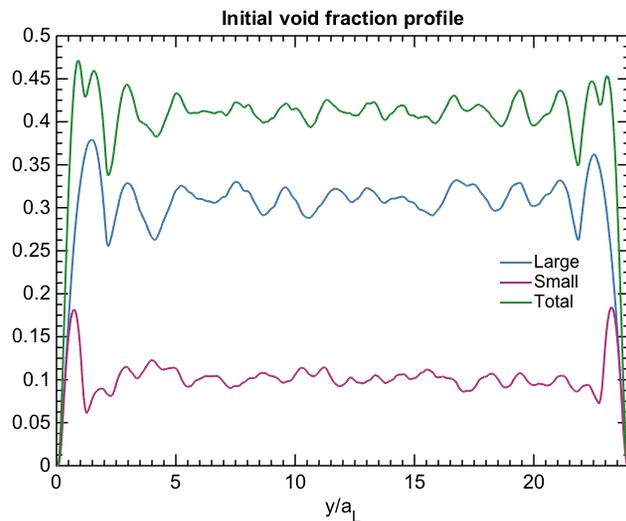
# FORCE COUPLING METHOD (FCM) FOR STOKES FLOW: BIDISPERSED RESULTS

- Developing Poiseuille flow in a channel.
- Flux migration, counter to  $\nabla\phi$  but in direction of decreasing shear
- $\Sigma_{22}^P$  creates a “body force” driving the flux
- Interested in the role of forces driving the migration (contact force versus lubrication) and instantaneous dynamics
- How does this change when the particles are different sizes?

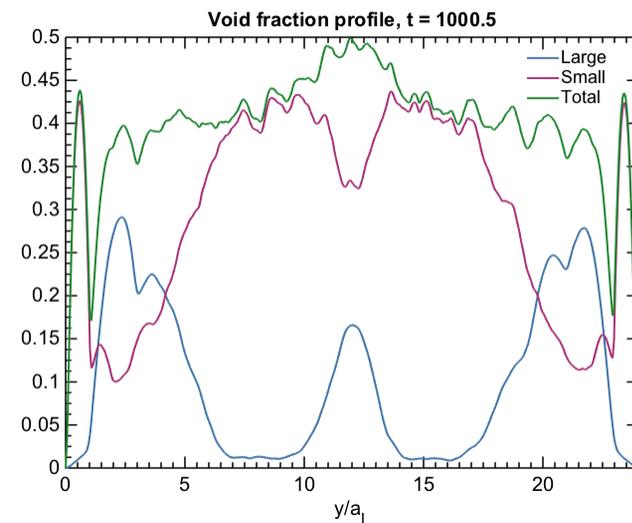
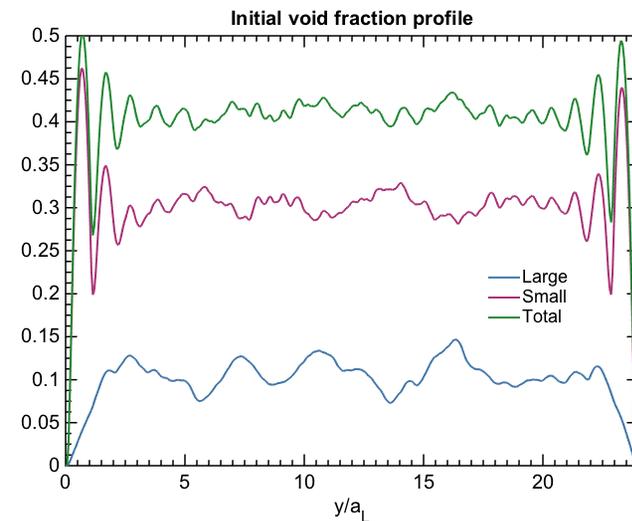


# FORCE COUPLING METHOD (FCM) FOR STOKES FLOW: BIDISPERSED RESULTS

$$\phi_L = 30\%, \phi_S = 10\%$$



$$\phi_L = 10\%, \phi_S = 30\%$$



- Uses low-order force multipole expansions to represent the particles.

$$\nabla p = \mathbf{f}^D + \mu \nabla^2 \mathbf{u} + \sum_{n=1}^{N_p} \{ \mathbf{F}^n \Delta_M(\mathbf{r}^n) + (G^n \cdot \nabla) \Delta_D(\mathbf{r}^n) \}$$

$$\nabla \cdot \mathbf{u} = 0$$

$$\Delta_M(\mathbf{r}) = \frac{1}{(2\pi\sigma_M^2)^{3/2}} \exp\left(-\frac{r^2}{2\sigma_M^2}\right), \sigma_M = a/\sqrt{\pi}$$

$$\Delta_D(\mathbf{r}) = \frac{1}{(2\pi\sigma_D^2)^{3/2}} \exp\left(-\frac{r^2}{2\sigma_D^2}\right), \sigma_D = a/(6\sqrt{\pi})^{1/3}$$

- Translational and angular velocities obtained from weighted volume integrals.

$$\mathbf{v}_i = \int (u)_i(\mathbf{x}) \Delta_M(\mathbf{r}) d^3 \mathbf{x}, \quad \Omega_i = \int \epsilon_{ijk} \frac{\partial \mathbf{u}_k}{\partial \mathbf{x}_j}(\mathbf{x}) \Delta_D(\mathbf{r}) d^3 \mathbf{x}.$$

- Mobility problem:

$$\begin{bmatrix} U - U^\infty \\ \Omega - \Omega^\infty \\ -E^\infty \end{bmatrix} = M^{FCM} \begin{bmatrix} F \\ T \\ S \end{bmatrix}$$

# FCM FOR STOKES FLOW: NEAR-FIELD INTERACTIONS

- Short range contact forces
- Lubrication viscous forces: Pairwise addition of two-body resistance matrices<sup>1</sup>
- Use preconditioned conjugate gradient method for solving  $R^{-1}$  terms. Two steps: outer iteration for FCM dipole terms, inner iteration for local lubrication forces and torques—important for closely clustered particles.<sup>2</sup>
- **Condition number of  $\mathcal{R}$  scales like  $10^3/\epsilon$ .**
- **Condition number of  $M_{SE}$  scales like  $(a_L/a_s)^3$**

$$\begin{aligned}\mathbf{F}^{Lub} &= \mathcal{R}\mathbf{U} \\ \mathbf{U}^T &= (\mathbf{V}^T, \Omega^T) \\ \mathcal{R} &= \begin{bmatrix} R_{VF} & R_{\Omega F} \\ R_{VT} & R_{\Omega T} \end{bmatrix}\end{aligned}$$

$$\begin{bmatrix} U - U^\infty \\ \Omega - \Omega^\infty \\ -E^\infty \end{bmatrix} = M^{FCM} \begin{bmatrix} F \\ T \\ S \end{bmatrix}$$

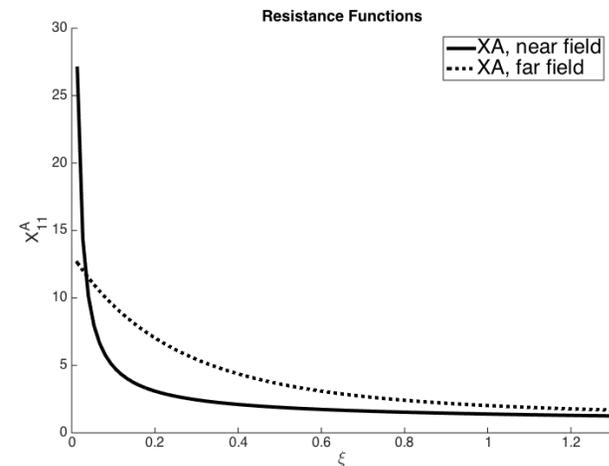


FIGURE: Sample resistance functions<sup>3</sup>.  $\xi = \epsilon/\langle a \rangle$

<sup>1</sup>Brady & Bossis, Ann. Rev. Fluid Mech. 20 (1998)

<sup>2</sup>Yeo & Maxey, J. Fluid Mech. 682 (2011)

<sup>3</sup>Jeffrey & Onishi, J. Fluid Mech. 139 (1984)

# MOVING LEAST SQUARES (MLS) BASIC IDEA

We want to approximate a function  $u$  near a point  $x_i$ . Define

$$u_h(x; x_i) = q^*(x_i)$$

where  $q^*$  is the solution to a weighted  $l_2$  optimization problem:

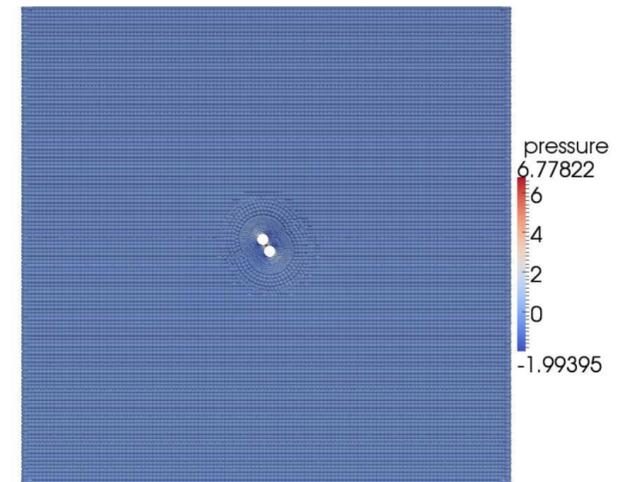
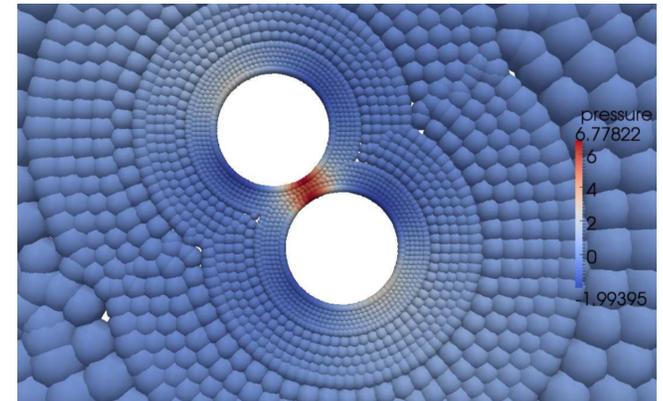
$$q^* = \arg \min_{q \in \pi_m} \sum_{i=1}^N [u(x_j) - q(x_j)]^2 W_{ij}$$

Operator  $D^\alpha$  is found by applying  $D^\alpha$  to the reconstruction:

$$D^\alpha \mathbf{u}_i \approx D_h^\alpha \mathbf{u}_i := D^\alpha q^*(\mathbf{x}_i)$$

- Recently developed Staggered MLS scheme for numerical solutions of Stokes flow
- Polynomial interpolants are used to represent the flow using least squares minimization
- High order accurate (4th or 6th order easily obtained by changing the order of the polynomial interpolants.)
- Force-free and torque-free colloids with position  $\mathbf{X}_i$ , orientation  $\Theta_i$ , and boundary  $\partial\Omega_i$ .

$$\begin{cases} -\nu \nabla^2 \mathbf{u} + \nabla p = \mathbf{f} & \mathbf{x} \in \Omega \\ \nabla \cdot \mathbf{u} = 0 & \mathbf{x} \in \Omega \\ \mathbf{u} = \mathbf{w} & \mathbf{x} \in \partial\Omega \\ \mathbf{u} = \dot{\mathbf{X}}_i + \dot{\Theta}_i \times (\mathbf{x} - \mathbf{X}_i) & \mathbf{x} \in \partial\Omega_i \end{cases}$$



**FIGURE:** Point adaptivity for colloids interacting under shear flow. Particle adaptivity visualized by rendering spheres at each point with diameter proportional to  $\epsilon_j$

<sup>4</sup>N. Trask, Ph.D. thesis (2015)

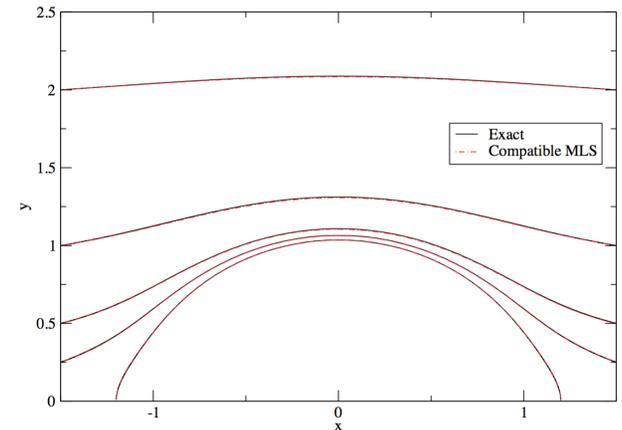
# MLS FOR STOKES FLOW

Choose  $\mathbf{u}$  in the space of divergence free vector fields.

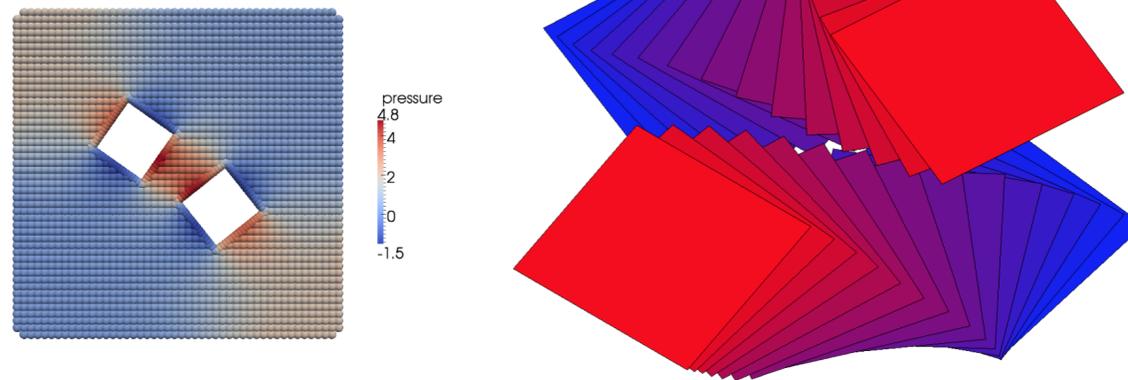
$$\begin{cases} \nu \nabla \times \nabla \times \mathbf{u} + \nabla p = \mathbf{f} & \mathbf{x} \in \Omega \\ \mathbf{u} = \mathbf{w} & \mathbf{x} \in \partial\Omega \end{cases}$$

$$\begin{cases} \nabla^2 p = \nabla \cdot \mathbf{f} & \mathbf{x} \in \Omega \\ \partial_n p + \nu \hat{\mathbf{n}} \cdot \nabla \times \nabla \times \mathbf{u} = \hat{\mathbf{n}} \cdot \mathbf{f} & \mathbf{x} \in \partial\Omega \end{cases}$$

$$\begin{cases} \mathbf{u} = \dot{\mathbf{X}}_i + \dot{\Theta}_i \times (\mathbf{x} - \mathbf{X}_i) & \mathbf{x} \in \partial\Omega_i \\ m_i \ddot{\mathbf{X}}_i = \int_{\partial\Omega_i} \sigma_v \cdot d\mathbf{A} \\ I_i \ddot{\Theta}_i = \int_{\partial\Omega_i} (\mathbf{x} - \mathbf{X}_i) \times \sigma_v \cdot d\mathbf{A} \end{cases}$$



**FIGURE:** Exact and MLS results for trajectory of particles in shear flow for varying initial colloid configuration.



**FIGURE:** Square particles of unit size in shear flow.

- Identify a virtual dual face with each edge and a virtual cell with each node.

$$\text{div}_h : E \rightarrow N$$

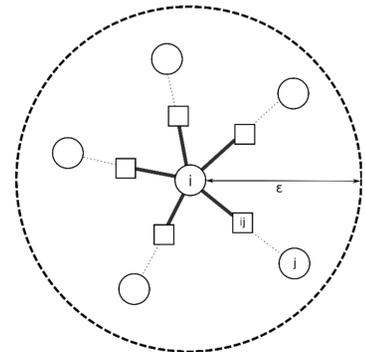
$$\text{grad}_h : N \rightarrow E$$

$$\text{grad}_h(\phi)_{ij} = \int_{e_{ij}} \nabla \phi \cdot ds = \phi_j - \phi_i$$

- To define  $\text{div}_h$ , first define the radial component function  $\mathbf{u}_{i \rightarrow}(\mathbf{x}) := \mathbf{u}(\mathbf{x}) \cdot 2(\mathbf{x} - \mathbf{x}_i)$ .
- For sufficiently smooth  $\mathbf{u}$ ,  $\mathbf{u}(\mathbf{x}_i) = \frac{1}{2} \nabla \mathbf{u}_{i \rightarrow}(\mathbf{x}_i)$  and  $\nabla \cdot \mathbf{u}(\mathbf{x}_i) = \frac{1}{4} \nabla \cdot \nabla \mathbf{u}_{i \rightarrow}(\mathbf{x}_i)$  hold.
- Reconstruct the vector fields and divergences at nodes by sampling component functions at edges:

$$q^* = \arg \min_{q \in \pi_m} \left\{ \sum_j [\mathbf{u}(\mathbf{x}_{ij}) \cdot 2(\mathbf{x}_{ij} - \mathbf{x}) - q(\mathbf{x}_{ij})]^2 W_{ij} \right\}$$

$$\mathbf{u}_h(\mathbf{x}_i) = \frac{1}{2} \nabla q^*(\mathbf{x}_i), \quad \nabla_h \cdot \mathbf{u}(\mathbf{x}_i) = \frac{1}{4} \nabla \cdot \nabla q^*(\mathbf{x}_i)$$



- Viscous operator:

$$\nabla \times \nabla \times \mathbf{u}(\mathbf{x}_i) \approx \nabla \times \nabla \times_h \mathbf{u}(\mathbf{x}_i) := \nabla \times \nabla \times \mathbf{v}^*(\mathbf{x}_i)$$

- Standard discretization over this basis:

$$\mathbf{v}^* = \arg \min_{\mathbf{v} \in \pi_m^{div}} \left\{ \sum_{j=1}^{N_p} [\mathbf{u}(\mathbf{x}_j) - \mathbf{v}(\mathbf{x}_j)]^2 W_{ij} \right\}$$

- Because of the form of minimizing a polynomial, we can write each quantity as a linear combination:

$$\nabla_h^2 p_i = \sum_{j \in (W_{ij})} \alpha_{ij}^1 p_j$$

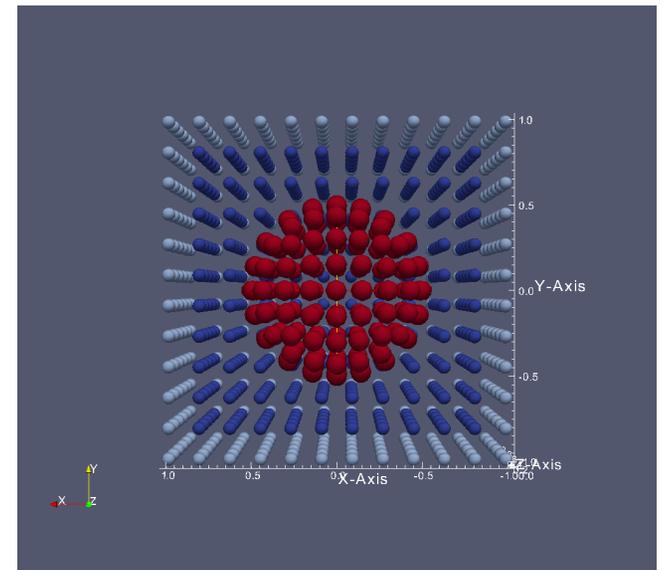
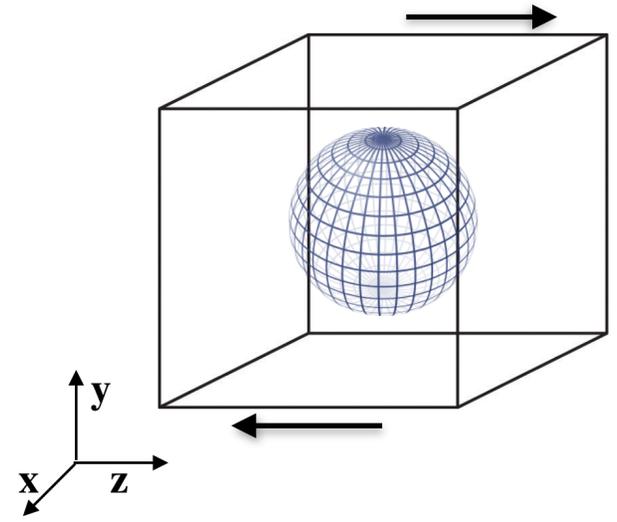
$$\nabla_h p_i = \sum_{j \in (W_{ij})} \alpha_{ij}^2 p_j$$

$$\nabla \times \nabla \times_h \mathbf{u}_i = \sum_{j \in (W_{ij})} \alpha_{ij}^3 \mathbf{u}_j$$

- Dirichlet boundary conditions are reinforced on the global matrix.
- Lack of symmetry makes it difficult to provide divergence free. Only divergence free in the local polynomial reconstruction.

# SPHERE IN COUETTE FLOW

- Sphere with radius  $r$  in a box  $\Omega = [-1, 1]^3$ .
- Boundary conditions:  $u = (0, 0, y)$  on  $\partial\Omega$ .



# SPHERE IN COUETTE FLOW

$$\Omega_x = \frac{1}{2} = 0.5$$

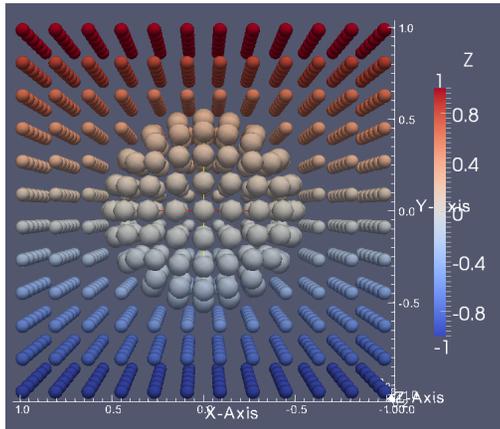


FIGURE:  $N = 12^3$ ,  $\Omega_x = 0.500684$

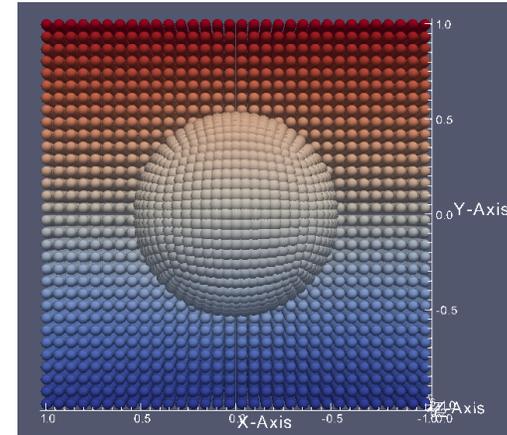


FIGURE:  $N = 32^3$ ,  $\Omega_x = 0.500149$

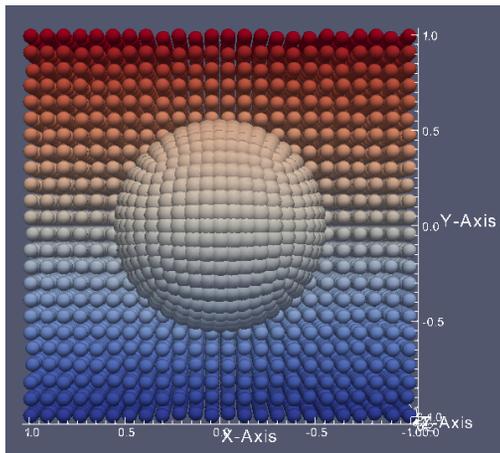


FIGURE:  $N = 24^3$ ,  $\Omega_x = 0.496785$

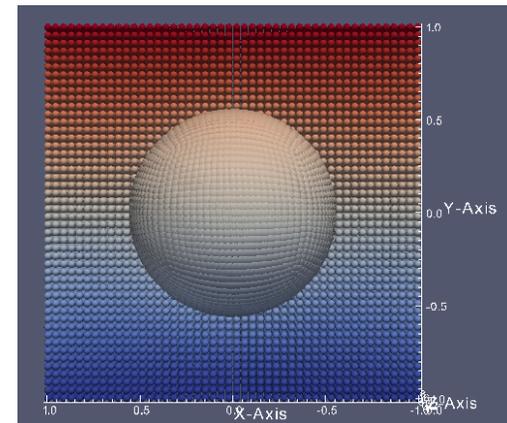
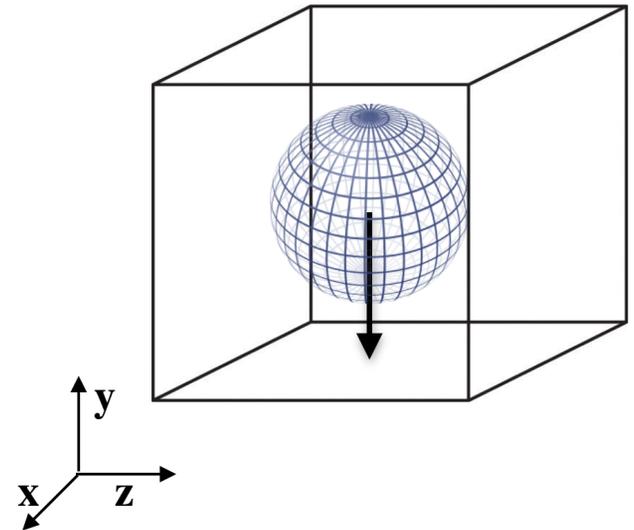


FIGURE:  $N = 48^3$ ,  $\Omega_x = 0.499069$

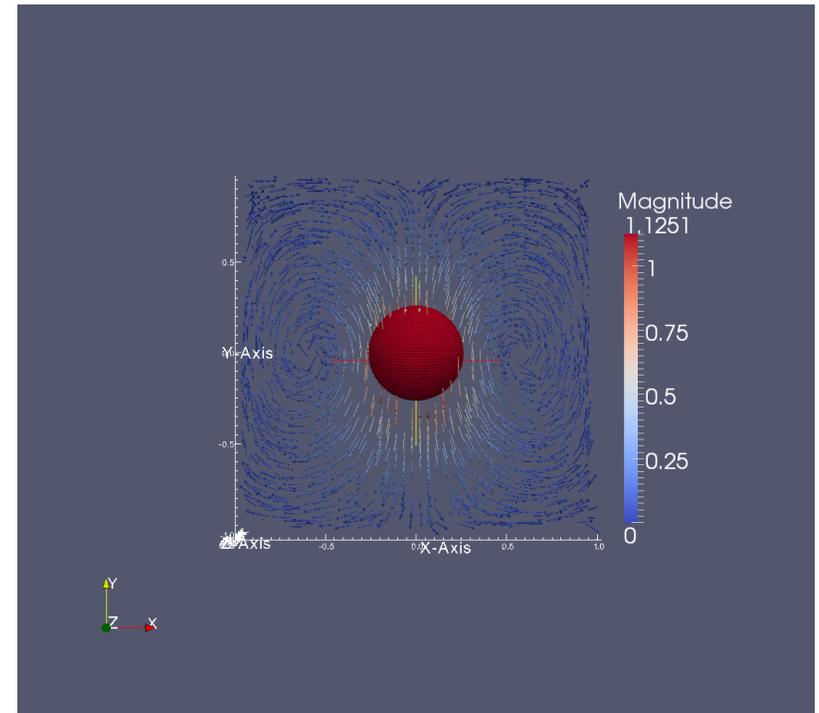
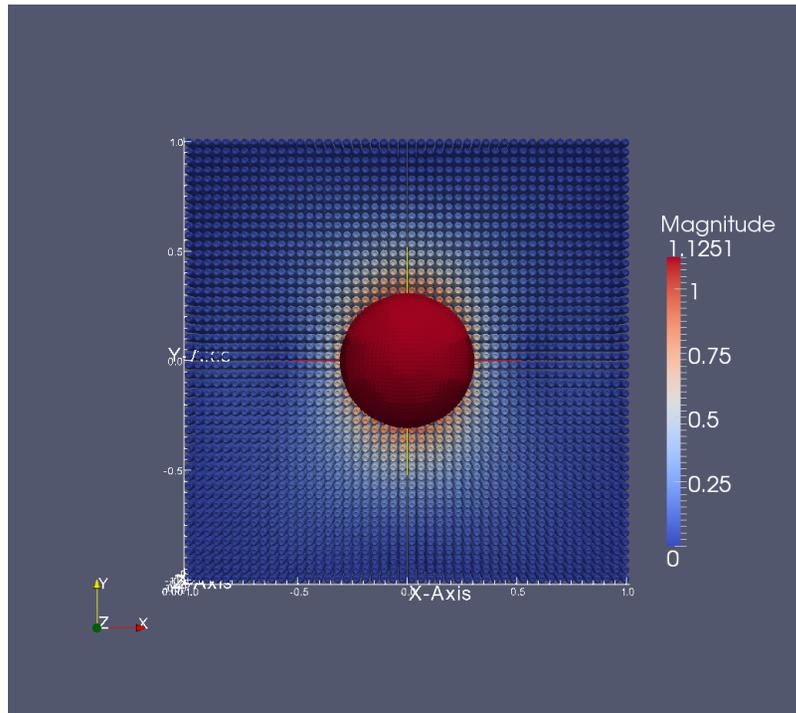
# SPHERE SETTLING

- Sphere with radius  $a$  in a box  $\Omega = [-1, 1]^3$ .
- Boundary conditions:  $u = (0, 0, 0)$  on  $\partial\Omega$ .
- Body force  $F = (0, -6\pi\mu a U_0, 0)$  imposed on the sphere.



# SPHERE SETTLING

$$N = 48^3$$



- Have fast and stable methods using only the graph of neighbor connectivity.
- Applications include irregular domains and non-spherical particle shapes with higher order accuracy
- Future work: coupling FCM and MLS

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